SIMPOSYUM ON "SITING OF NEW NUCLEAR POWER PLANTS AND IRRADIATED FUEL FACILITIES"

LAS-ANS / CNEA / AATN – Buenos Aires-Argentina

"THE SEISMOTECTONIC ENVIRONMENT OF FUKUSHIMA ACCIDENT-LESSONS LEARNED"

Antonio R. GODOY Managing Director-James J. Johnson & Associates 24 June 2013

FUKUSHIMA DAIICHI NPP (F1)



INTRODUCTION

FUKUSHIMA ... The first nuclear accident caused by a combination of <u>extreme external</u> <u>events</u> ...

- •The seismotectonic environment, the earthquake, the tsunami
- The plant damage and response
- •The nuclear accident
- The management of the accident
- The radiological consequences
- The management of the emergency
- •The actions by the world nuclear community

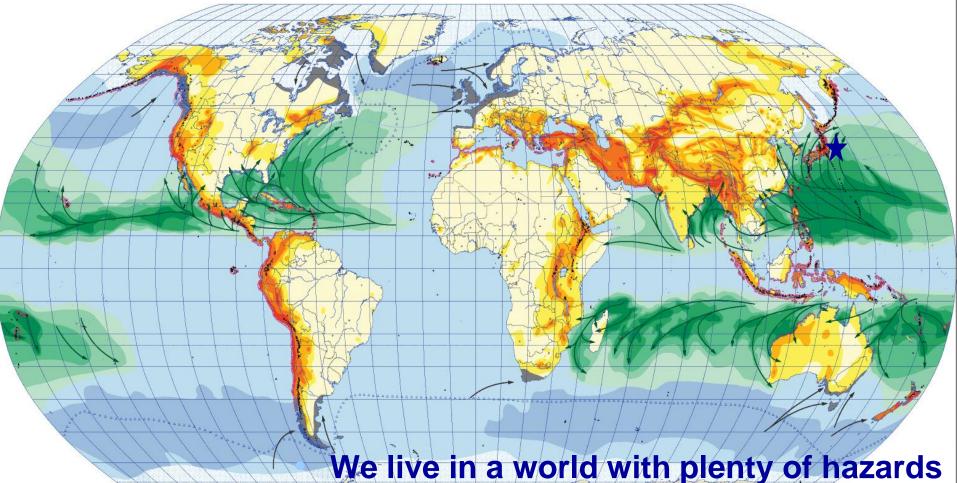
- A COMPLEX SCENARIO of COMBINATION of EXTREME EXTERNAL EVENTS AFFECTING SEVERAL NPPs and LEADING to a NUCLEAR ACCIDENT:
 - An earthquake of Magnitude 9 that did not produce apparent significant damage to the nuclear installations,
 - A tsunami, ~45 minutes later that flooded the Tokai 2, Fukushima Daiichi and Fukushima Daini sites,
 - Hydrogen explosions, a few hours-days later,
 - Aftershocks (. . . thousands), continuously, and
 - A region devastated with major damage to infrastructure and about 25000 casualties.

Chronology of Major Events at Fukushima Daiichi Unit 1

Before the earthquake		In rated output operation
March 11, 2011	14:46	Great East Japan Earthquake
		Off-site power lost
		Reactor scram
	14:47	All control rods fully inserted
		Emergency DG startup (circuit breaker actuated)
	14:52	Isolation condenser startup
	15:41	Station black out due to the tsunami (subsequent AM response)
		Main Control Room power supply cut off
		Instrumental power supply cut off
March 12	5:46	Freshwater injection using fire pumps started
	10:17	PCV venting started
	14:30	Decrease in D/W pressure. Successful containment vessel venting
	15:36	Hydrogen explosion

19:04 Sea water injection started

World Map of Natural Hazards



Earthquakes



Probable maximum intensity (MM: modified Mercalli scale) with an exceedance probability of 10% in 50 years (equivalent to "return period" of 475 years) for medium subsoil conditions

Volcanoes

- Last eruption before 1800 AD Δ
- Last eruption after 1800 AD Particularly hazardous volcanoes

Tsunamis and Storm Surges

- Tsunami hazard (seismic sea-wave)
 - Storm surge hazard
- Tsunami and storm surge hazard Surger 3

Tropical Storms and Cyclones



Zone 5: SS 5 (>= 250 km/h)

Probable maximum intensity (SS: Saffir-Simpson hurricane scale) with an exceedance probability of 10% in 10 years (equivalent to a "return period" of 100 years)

Principal tracks of tropical storms

Extratropical Storms/Winter Storms

- High extratropical storm hazard, mainly in winter
 - Principal tracks of extratropical storms

Other Natural Hazards

- Limit of iceberg drift ΔΔ
 - Pack ice (winter maximum)
- High seas with wave heights > 5 metres, exceedance probability 10% per year ("10-year wave")

Cities

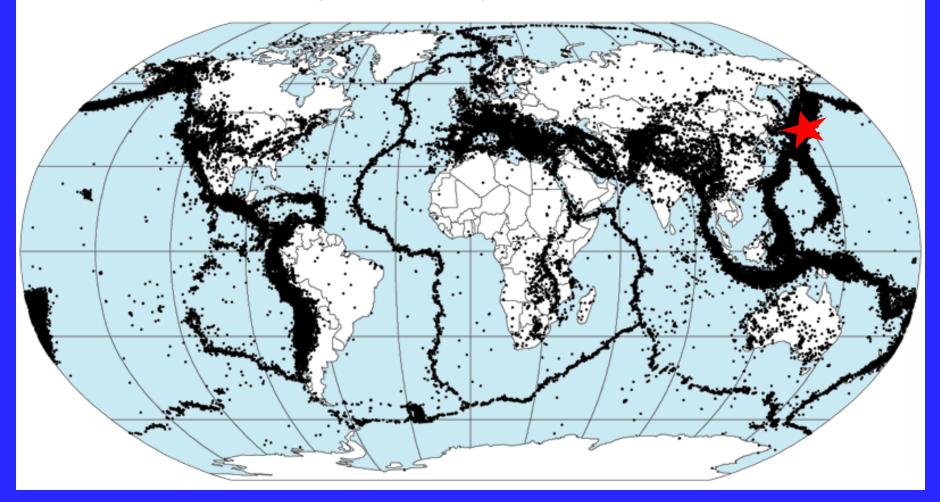
Derwar	> 1 million inhabitants
San Juan	100,000 to 1 million inhabitants
Maum	< 100,000 inhabitants
Batin	Capital city
Melbourne	Munich Re office
	San Juan Meun Barlin

Political Borders/Inland Waters

- State border
- State border, controversial (political borders not binding)
- River
- l ake manut
 - Previous extent of lake

Seattle Large city with "Mexico City effect"

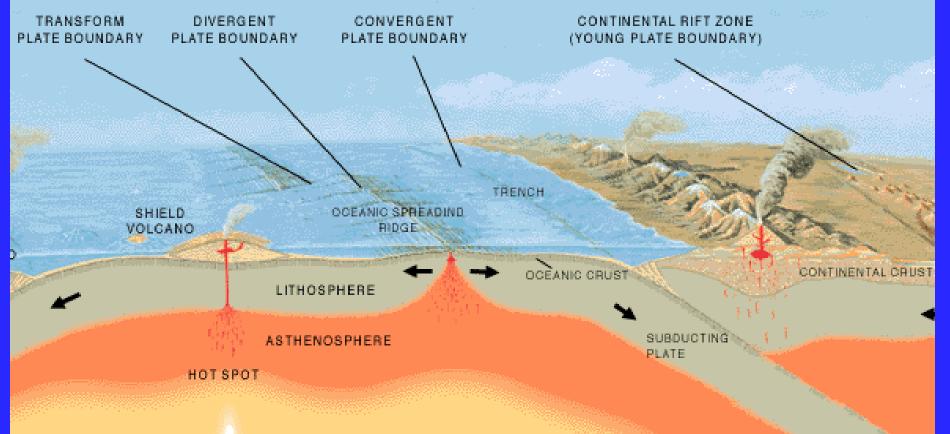
Preliminary Determination of Epicenters 358,214 Events, 1963 - 1998



Global Seismicity

NASA DATM

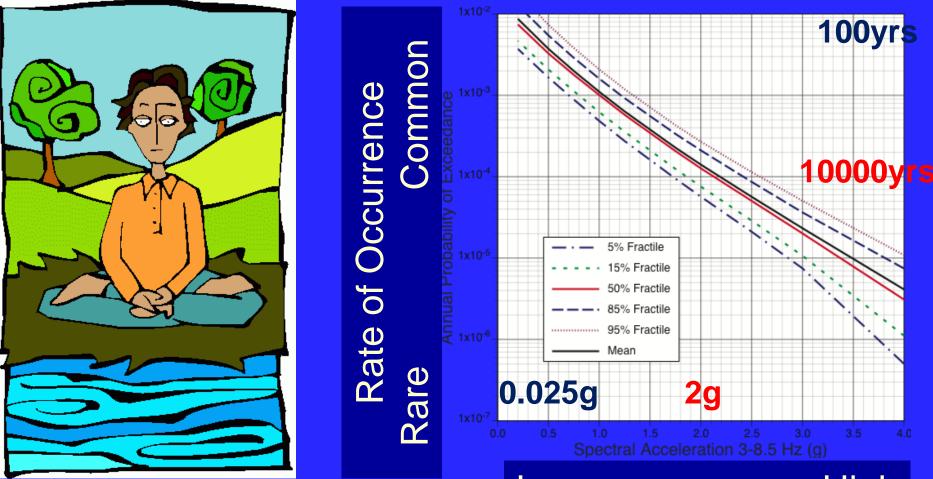
Plate Tectonics



The earthquakes are generated by faults rupture



Hazard levels calculated increase with time period of observation



Low High Shaking Level (pga)

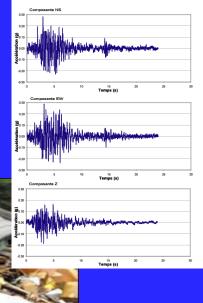
EARTHQUAKES AND "THE EARTHQUAKE"

THE SEISMIC HAZARDS:

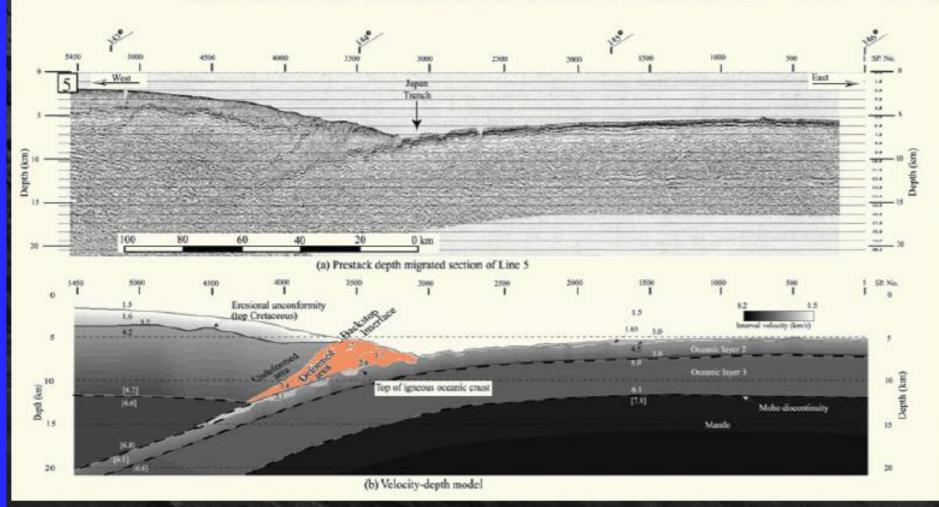
- Vibration of the ground
- Tectonic uplift/subsidence
- Landslides
- Soil failures
- Floods
- Fires







TSURU ET AL.: INTERPLATE COUPLING AT THE JAPAN TRENCH MARGIN ESE



cross section of Japan Trench (Tsuru et al., 2002) 40 m slip on 4° dipping thrust uplifts seafloor by 2.8 m. 40 m coseismic extrusion of the wedge uplifts by 3.5 m. 11 - 5

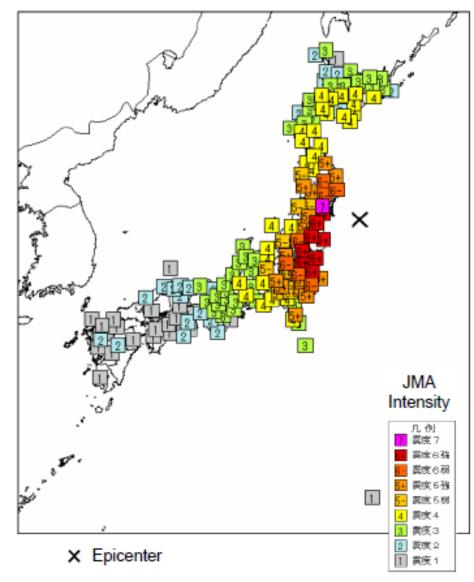
Overview of 2011 Great East Japan Earthquake

Commencement time: 14:46 on March 11, 2011

Epicenter: Off the coast of Sanriku

Earthquake specification: Mw 9.0 38° 6.2"N, 142° 51.6"E Depth: 24km

Distance of epicenter from plant site: Fukushima Daiichi 178km Fukushima Daini 183km



JMA Intensity map of main shock [From Japan Meteorological Agency]

ONAGAWA NPP

Tokyo

HIGASHI DORI NPP

Epicenter

FUKUSHIMA DAI-ICHI NPP

FUKUSHIMA DAI-NI NPP

Osaka

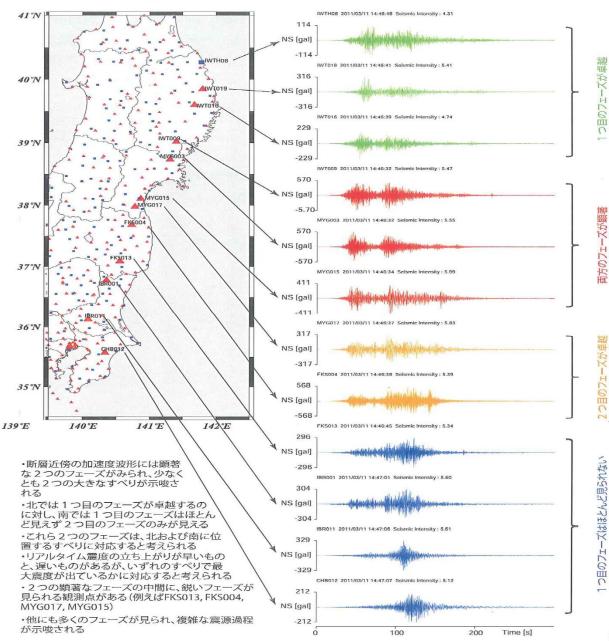
TOKAI DAI-NI NPP

Data SIO, NOAA, U.S. Navy, NGA, GEBCO

近地強震動波形に見られるフェーズの特徴

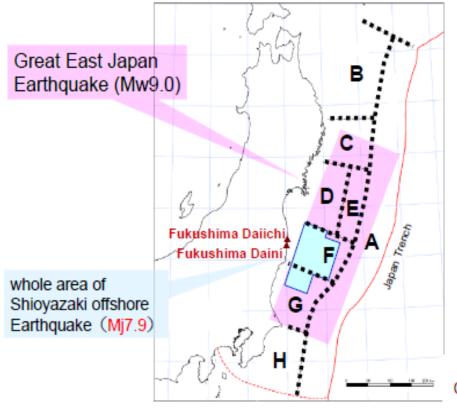
防災科学技術研究所資料

6



15

Source Fault of 2011 Great East Japan Earthquake



	Sea area	Estimated Mj			
Α	Sanriku offshore to Boso offshore along the Japan Trench	8.2			
в	Northern Sanriku offshore		3.0		
С	Middle Sanriku offshore	٢	N/A		
D	Miyagi pref. offshore	7.5	whole area		
Е	Close to the trench in southern Sanriku offshore	7.7 8.0			
F	Fukushima pref. offshore	7.4			
G	Ibaraki pref. offshore	6.7 - 7.2			
Н	Boso offshore	8.1			

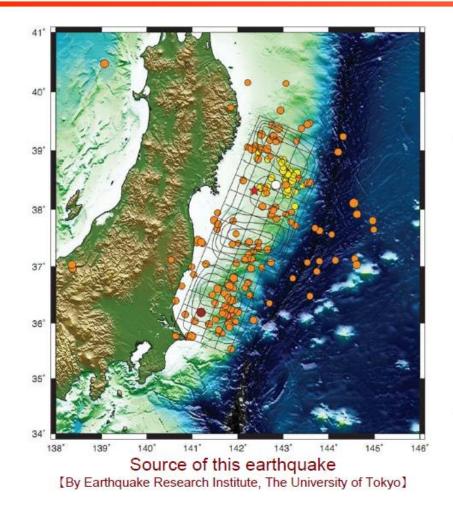
Comparison with areas assessed by the Earthquake Research Committee of the Headquarters for Earthquake Research Promotion [Revised by the Earthquake Research Committee (2009)]

Assessment of earthquakes for each area were conducted, but such a large interlock of multiple source areas as the earthquake was not conducted.

Even the Headquaters for Earthquake Research Promotion (HERP), a govermental organization, had not evaluated such a interlock as the earthquake.

Design basis ground motion Ss for Fukushima Daiichi and Fukushima Daini are determined under consideration of Mj7.9 earthquake, which was defined by interlocking large three source fault within the area "F" and is beyond the estimation for the area "F" by HERP (Mj7.4).

Source Fault of 2011 Great East Japan Earthquake



Largest earthquakes in the world [From USGS]

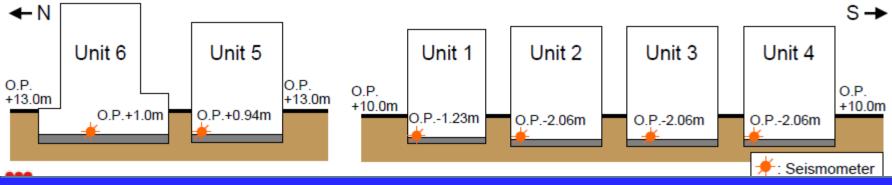
	Mw	
1960	Chile	9.5
<mark>1964</mark>	Alaska	9.2
2004	Sumatra	<mark>9.1</mark>
2011	Great East Japan	9.0
1952	Kamchatka	9.0

The March 11th earthquake occurred as multiple sources where earthquakes had occurred in the past interlocked, and the magnitude was the largest in recorded history for earthquakes occurring in the area surrounding Japan and the 4th largest in the world.

Records of Observations at Base-mat Slab of Reactor Building at Fukushima Daiichi NPS

	Maximun	n accelerati	on value	Maximum response acceleration value (Gal)					Static
	from observation records (Gal)			New design-basis seismic ground motion Ss			Original design-basis seismic ground motion		horizontal acceleration
	NS	EW	UD	NS	EW	UD	NS	EW	(Gal)
Unit 1	460	447	258	487	489	412	245		
Unit 2	348	550	302	441	438	420	250		
Unit 3	322	507	231	449	441	429	291	275	470
Unit 4	281	319	200	447	445	422	291	283	470
Unit 5	311	548	256	452	452	427	294	255	
Unit 6	298	444	244	445	448	415	495	500	

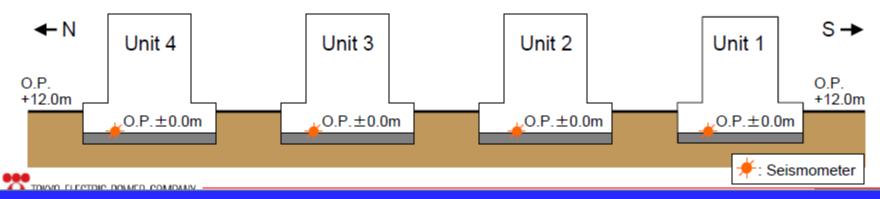
* indicates the observed value was beyond the response of Ss, the others were under the response of Ss.



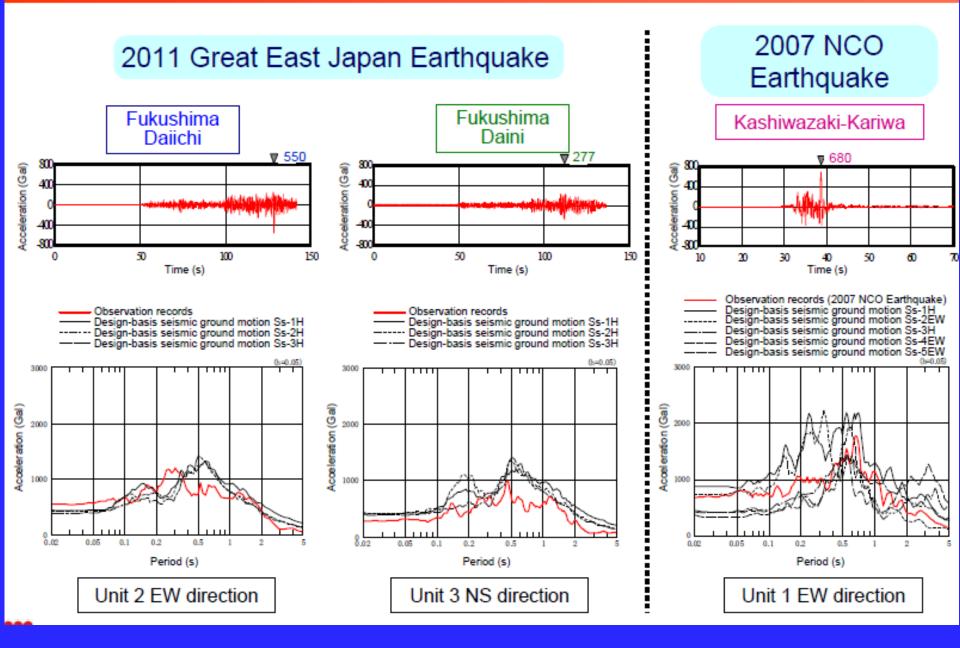
Records of Observations at Base-mat Slab of Reactor Building at Fukushima Daini NPS

	Maximun	n accelerat	ion value	Maximum response acceleration value (Gal)					Static
	from observation records (Gal)			New design-basis seismic ground motion Ss			Original design-basis seismic ground motion		horizontal acceleration
	NS	EW	UD	NS	EW	UD	NS	EW	(Gal)
Unit 1	254	230	305	434	434	512	372	372	
Unit 2	243	196	232	428	429	504	317	309	470
Unit 3	277	216	208	428	430	504	196	192	470
Unit 4	210	205	288	415	415	504	199	196	

* All observed maximum acceleration values were under the response of Ss.



Comparison of Great East Japan Earthquake and NCO Earthquake



TSUNAMIS AND "THE TSUNAMI" 1. What is a tsunami?







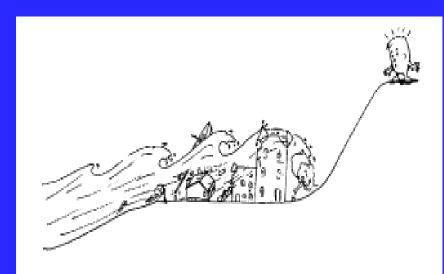


Tsunami Definition

Tsunami is a Japanese term, meaning wave ("nami") in a harbour ("tsu").

Terrae motus → Terremoto ↔ Earthquake Mare motus → Maremoto ↔ Tsunami





Tsunami Definition

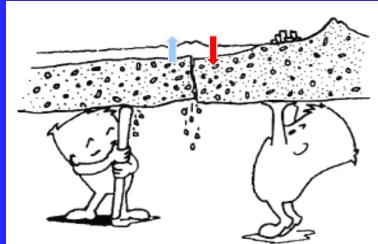
A tsunami is a wave ...

... is a series of traveling waves of extremely long length and period, ...

... generated by rapid (impulsive) disturbances usually associated with earthquakes occurring below the sea floor,

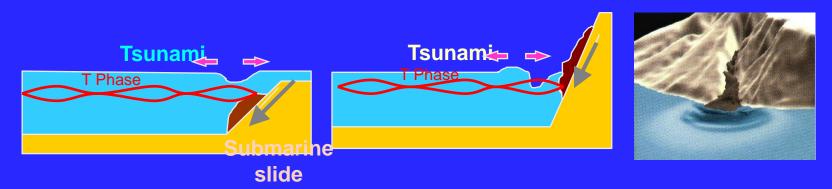
... near the coast of a sea or ocean, ... or near a large body of water.





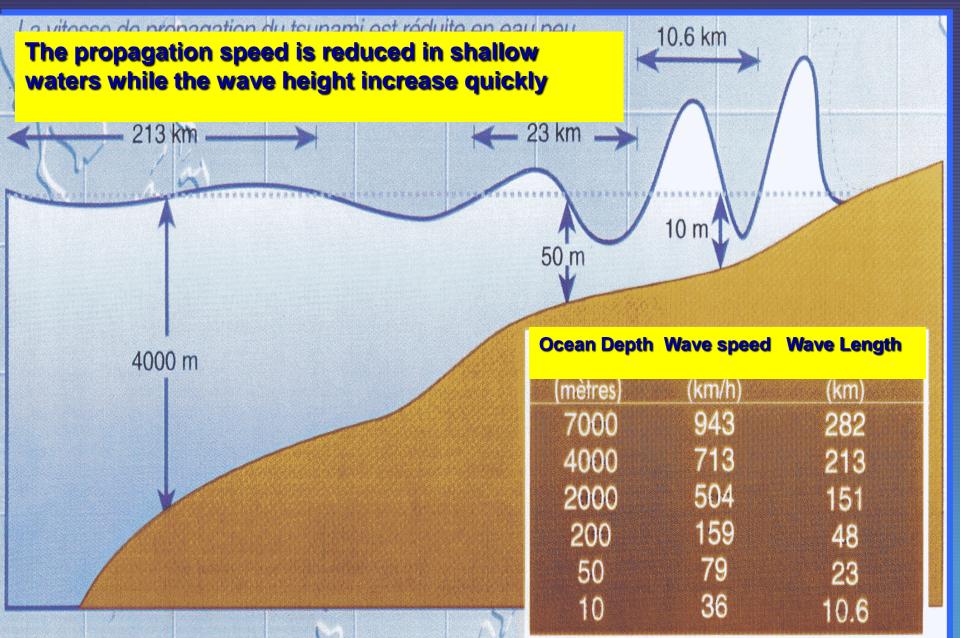
Tsunamis can also be generated by:

- Volcanic explosions or collapses,
- Submarine landslides,
- Coastal rock falls and landslides (triggered or not by earthquakes or volcanic eruptions),
- Large meteorite impacting the ocean.



Tsunamis have no connection with tides; the popular name of "tidal wave" Is entirely misleading.

Tsunami Process



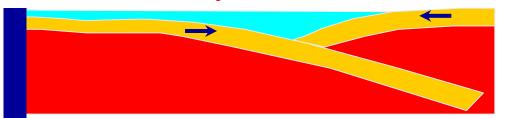
How is a tsunami generated?

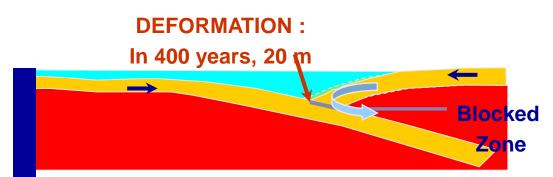
Subduction Zone:

1) ~400 Years ago

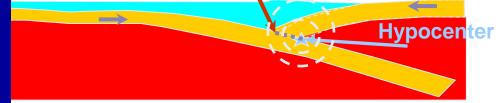
2) Just before earthquake

3) When the earthquake occurred, tsunami is generated RELATIVE MOTION → 5 cm/year ←





DISLOCATION : 20 m / several minutes Tsunami



The 3 stages of a tsunami

INUNDATION

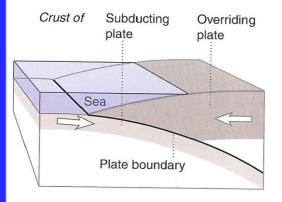
GENERATION

Three basic stages of tsunami behaviour:
1.Generation, in the subduction fault
2.Propagation, in the open sea, and
3.Inundation, when reachs the coast.

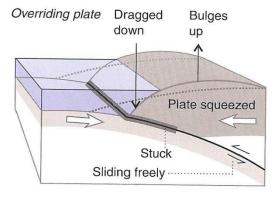
PROPAGATION

How we know that a tsunami happened years ago?

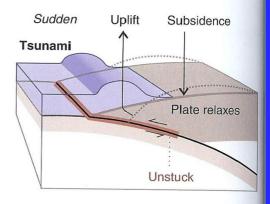
MAKING A TSUNAMI



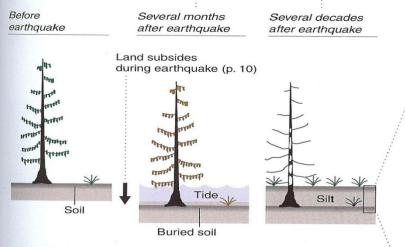
OVERALL, a tectonic plate descends, or "subducts," beneath an adjoining plate. But it does so in a stick-slip fashion.



BETWEEN EARTHQUAKES the plates slide freely at great depth, where hot and ductile. But at shallow depth, where cool and brittle, they stick together. Slowly squeezed, the overriding plate thickens.

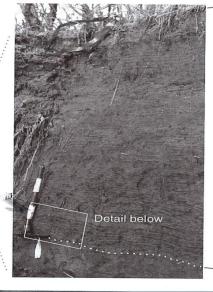


DURING AN EARTHQUAKE the leading edge of the overriding plate breaks free, springing seaward and upward. Behind, the plate stretches; its surface falls. The vertical displacements set off a tsunami.



By lowering land into a bay or river mouth, subsidence during an earthquake produces a lasting record of the earthquake's occurrence.

TIDAL SILT AND SAND ABOVE BURIED SOIL, TWENTYMILE RIVER



Ground surface in 1998

Tidal silt and sand, 1.5 m thick, mostly deposited in the first few years after the 1964 earthquake

 Ground surface before the earthquake

Tsunami Definitions

- Run-up > Maximum water level (2 to 3)
- Inundation
- Maximum Water Level
- Water Level at shoreline



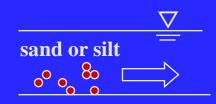
Tsunami stripped forested hills of vegetation leaving clear marker of fsunami runup, Banda Aceh, 26 December 2004 Sumutra tsunami. Photo courtesy of Yuichi Nishimura, Hokkado University.



Tsunamis Direct Effects

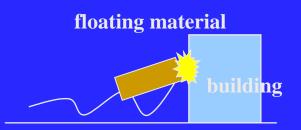
 Variation (+ / -) of Water Level,





- Sand Movement,
- Water dynamic effects: Wave Pressure / Force,
- Floating Material (debris of all types),





General Effects of External Flooding

Common cause failure for safety related systems:

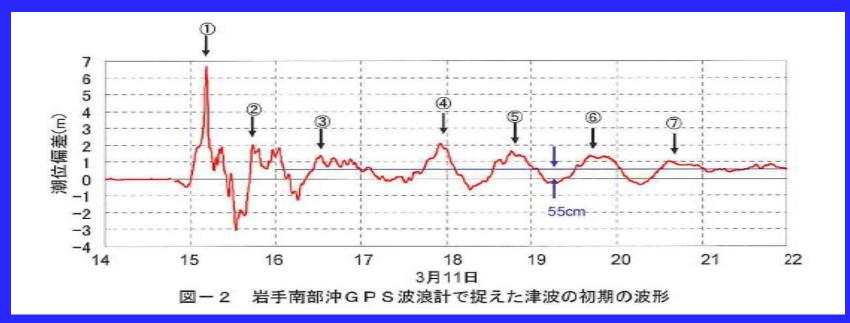
- Cooling Water Systems
- Emergency power supply system.
- **Electric switchyard.**
- Loss of external connection to the electric power grid.

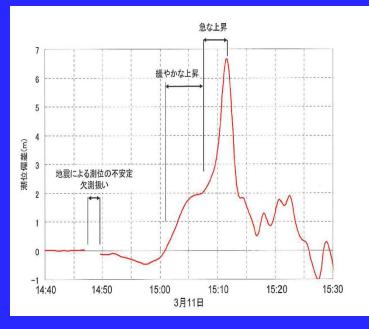
Infiltration of water to internal areas of the plant:

- Increase of water pressure on walls and foundations.
- Deficiencies in drainage system, causing flooding at the plant facilities with consequent large scale damage.
- Dynamic effects of the water and erosion at the site boundary.
- Effects on communication and transport networks around the plant site.

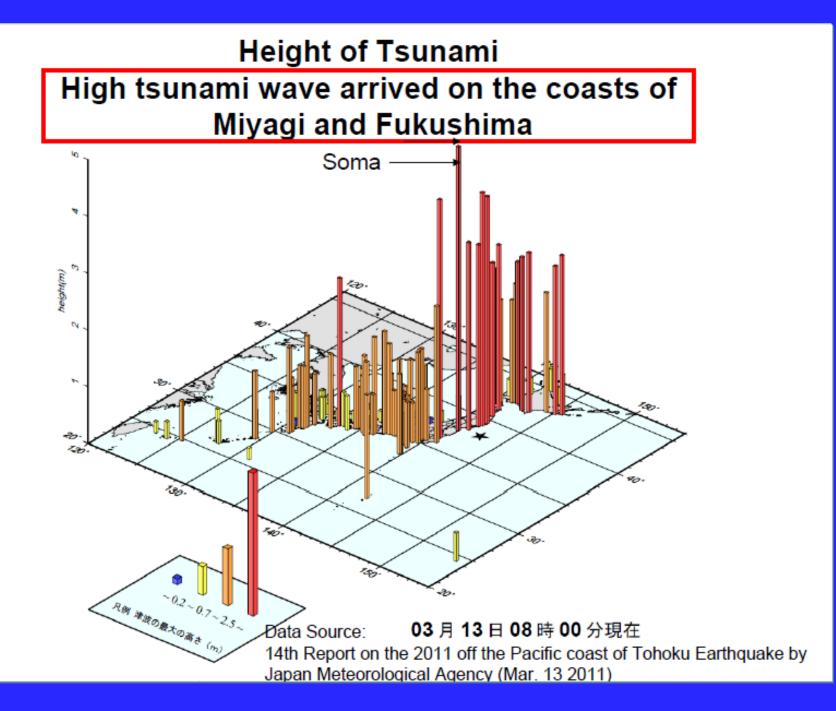
TSUNAMIS

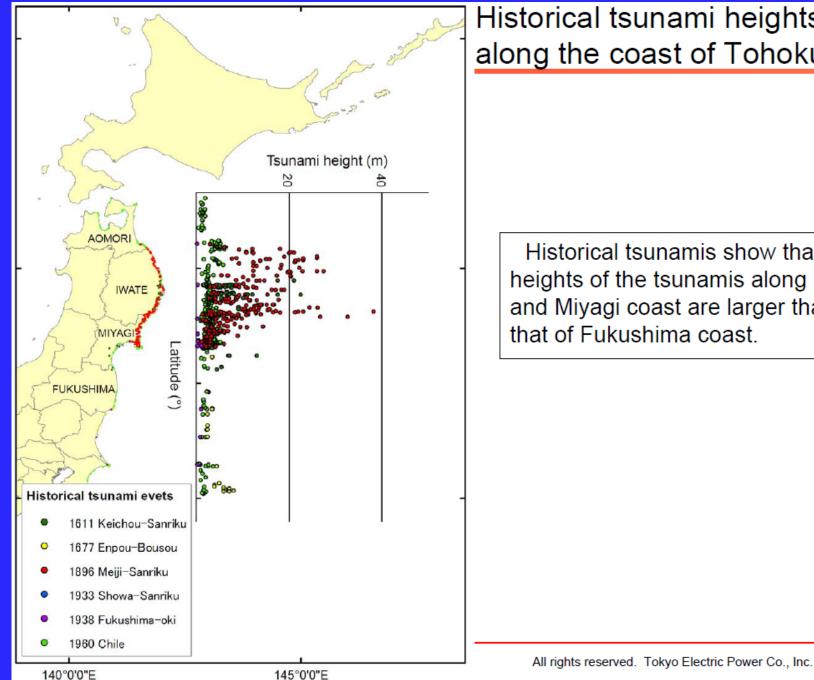
2. The 11 March 2011 Tsunami ... the "reality"





The 11-03-2011 Tsunami waves

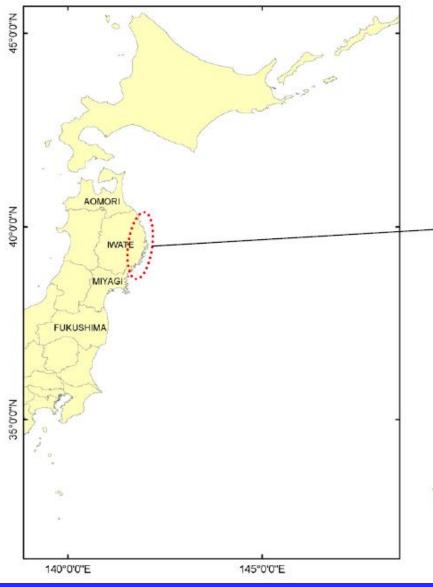




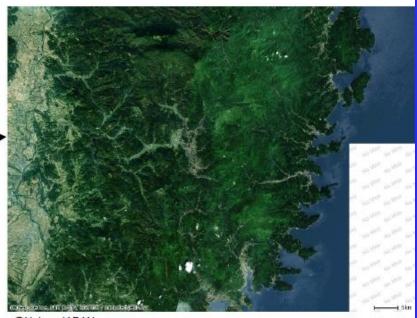
Historical tsunami heights along the coast of Tohoku area

Historical tsunamis show that the heights of the tsunamis along lwate and Miyagi coast are larger than that of Fukushima coast.

Topography of Iwate and Miyagi coast



The tsunami wave is amplified at bays in the ria-coast



©Yahoo JAPAN

The factor affecting the height of tsunami along Iwate and Miyagi coast

TSUNAMIS

3. The effects of 11 March 2011 Tsunami on the F1/F2 NPPs.

Trace of the Tsunami on March 11th, 2011.

(1)Inundation height

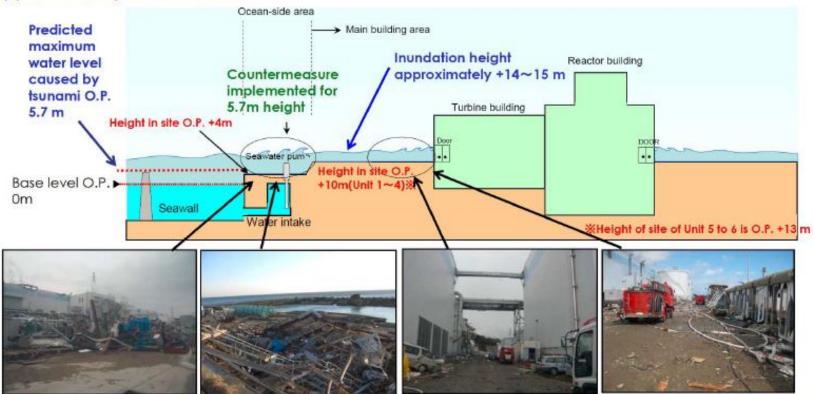
Approximately O.P. +14 to 15 m (inundation depth: approximately 4 to 5 m) in most of the ocean-side of main building area.

(2)Inundation area

Most of the ocean-side area (height of site: O.P. +4 m) and the main building area.

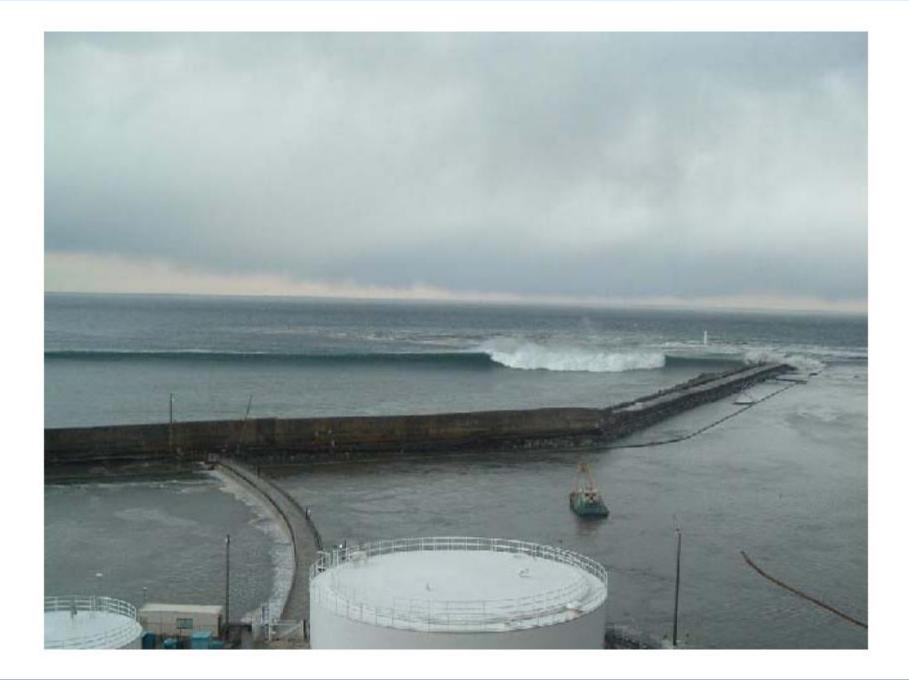
(3)Run-up height

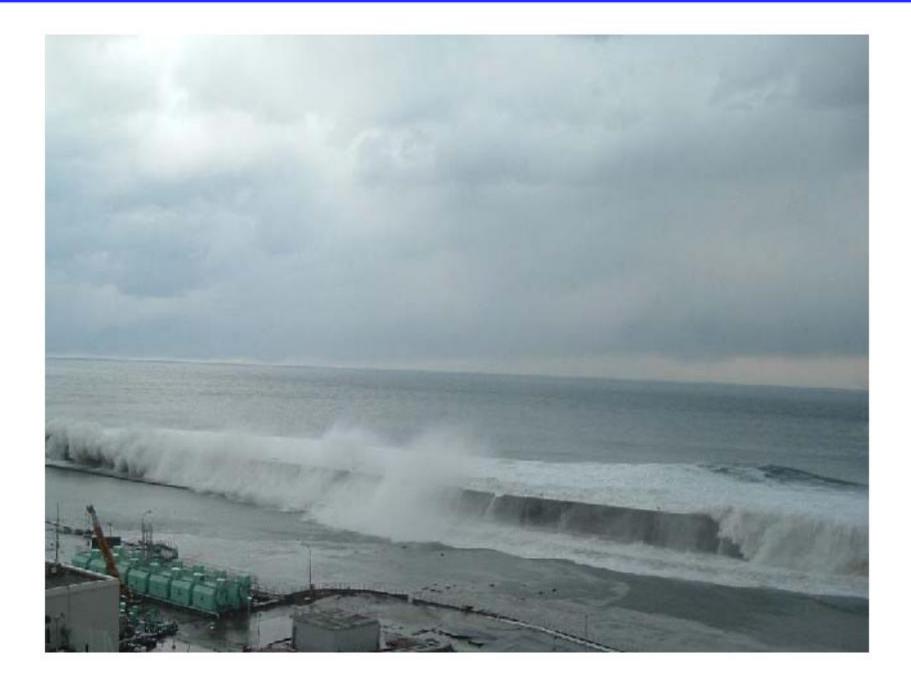
Approximately O.P. +14.5 m.





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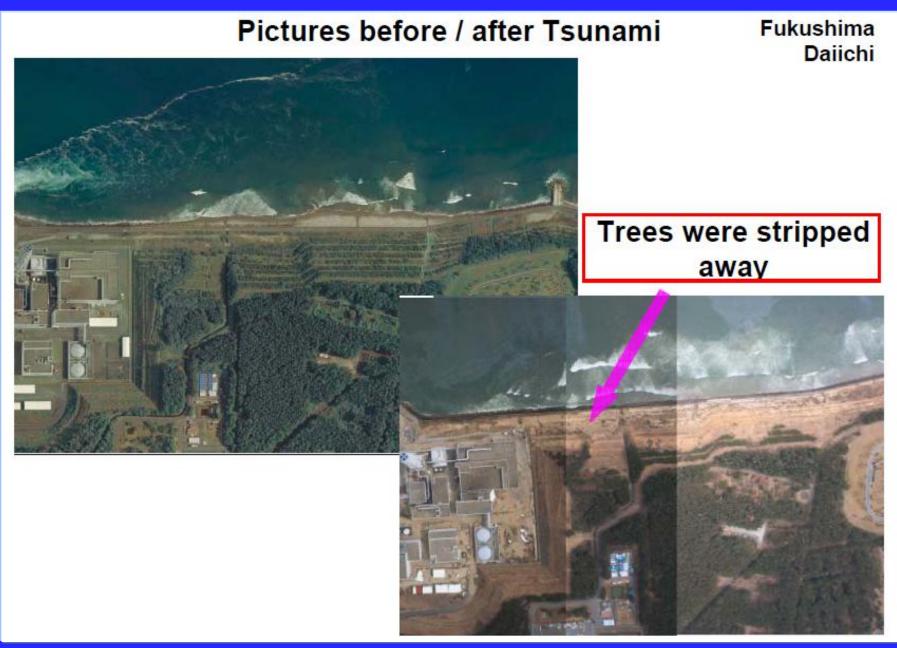




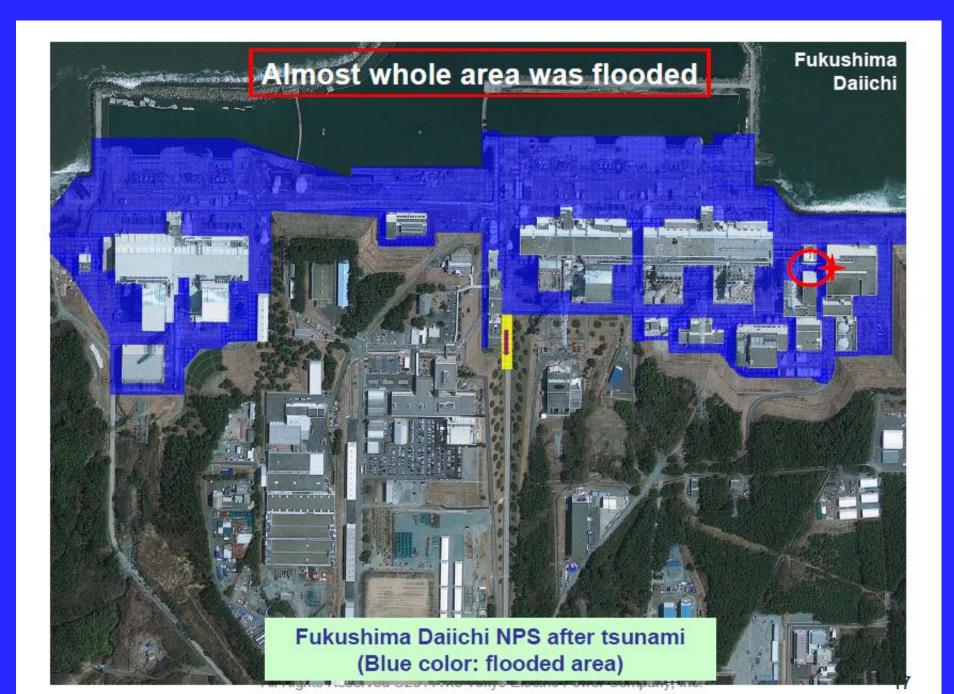


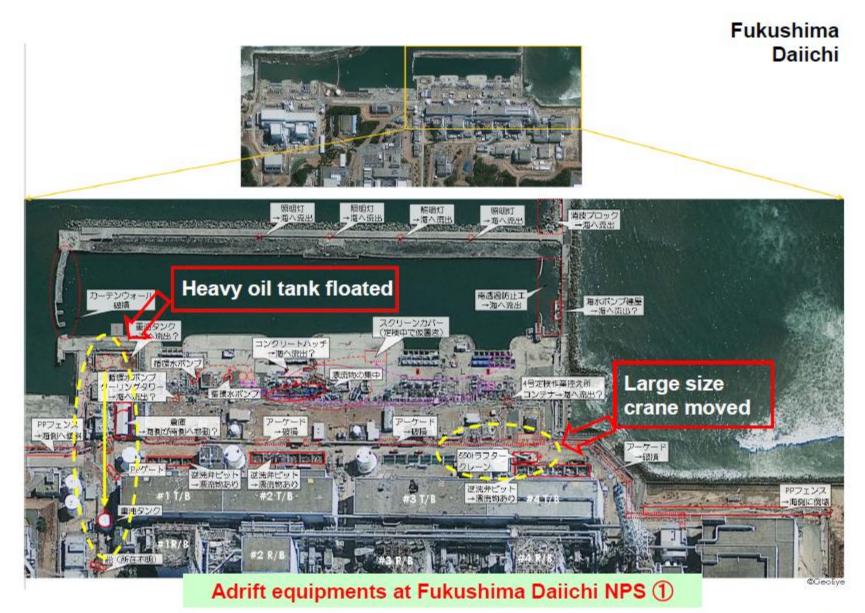














Adrift equipments at Fukushima Daiichi NPS (2)

@GeoEye

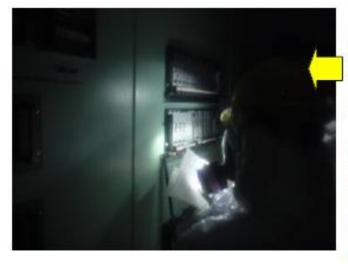


External factors that made field work difficult (inside the building)

As there was no power, work inside the building was conducted in complete darkness.

As there was no power, temporary instrument power had to be installed separately for each instrument.





Work in complete darkness Photo of the Service Building entrance taken from inside the building. Objects were scattered on the floor. <u>Temporary instrument</u> power

As there was no power, temporary batteries were connected and used as a power supply for instruments.

Monitoring by the assistant shift supervisor Confirmed readings in complete darkness using a light

Monitoring by the assistant shift supervisor

Condition of the assistant shift supervisor's desk. Monitoring in complete darkness wearing a full-face mask





External factors that made field work difficult (yard)

- During the initial response, there were several aftershocks, and work was conducted in extremely poor conditions, with uncovered manholes and cracks and depressions in the ground (in particular, nighttime work was conducted in the dark).
- · There were also many obstacles blocking access routes.



Depressions in roads, etc. Areas that were dangerous even to walk. Particularly dangerous at night.

Obstacles on access routes Fire hoses, etc., were laid around access routes. After the explosion, rubble and damaged fire tucks became additional obstacles.



Access to lay temporary power sources

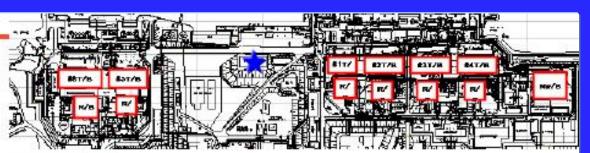
In order to enter the building, the large object delivery entrance was destroyed using heavy equipment.

Laying of temporary power sources

Employees other than electricity-related personnel helped in laying the cables.

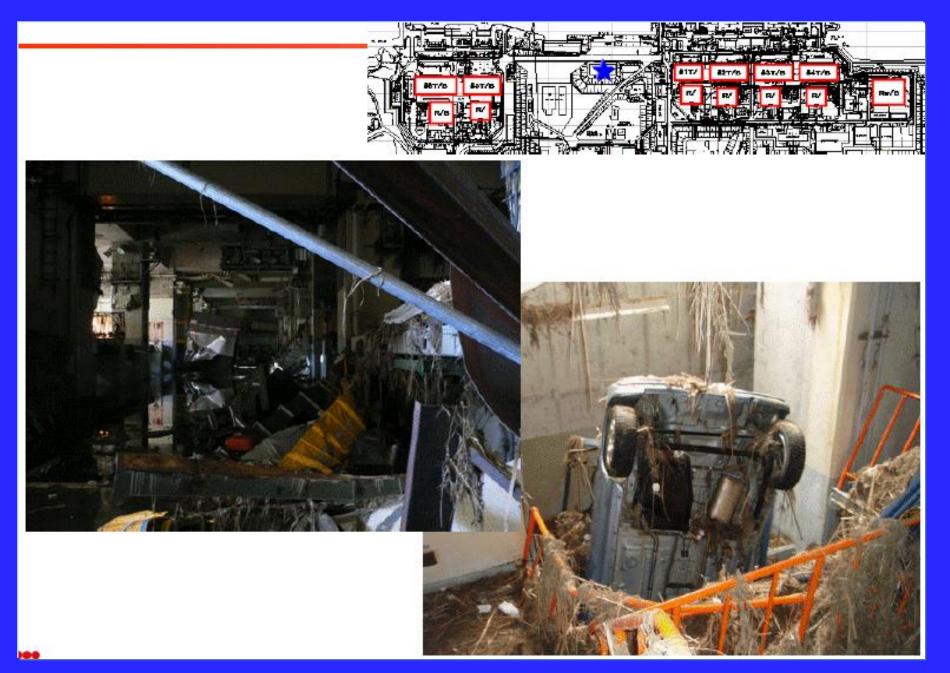






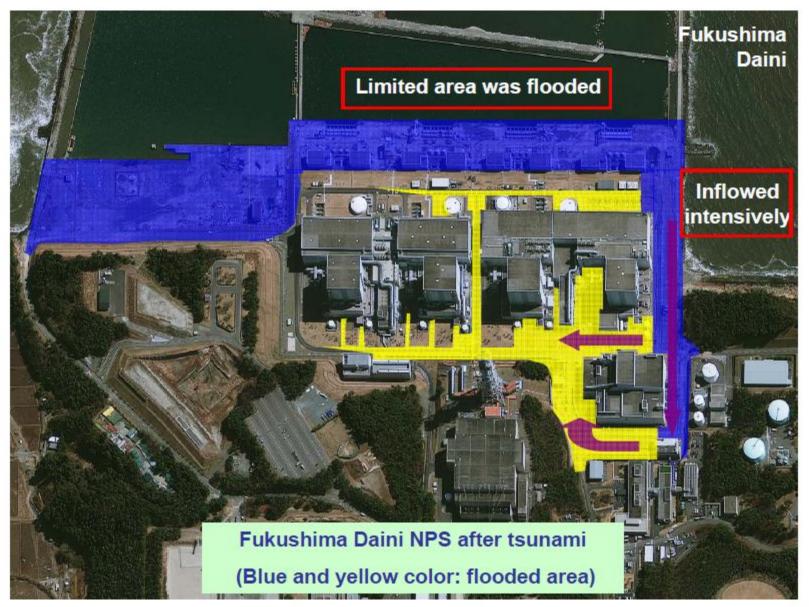






Fukushima Daini Assumed highest Inundation height apx. O.P. 7m tsunami water level (South of Unit 1 O.P. +14-15m) O.P.+5.2m Ocean-side Main building area area Reactor building Inundation height apx. O.P. +14-15m Assumed highest Safety measures has taken against tsunami water level 5.7m Tsunami height Turbine building O.P.+5.2m Site level Heat excl anger building O.P. +4m •• Base level O.P.0m Site level O.P. +12m breakwater Water intake 夏水町 載タン attripping the 0112334

Tsunami Attack at Fukushima Daini NPS



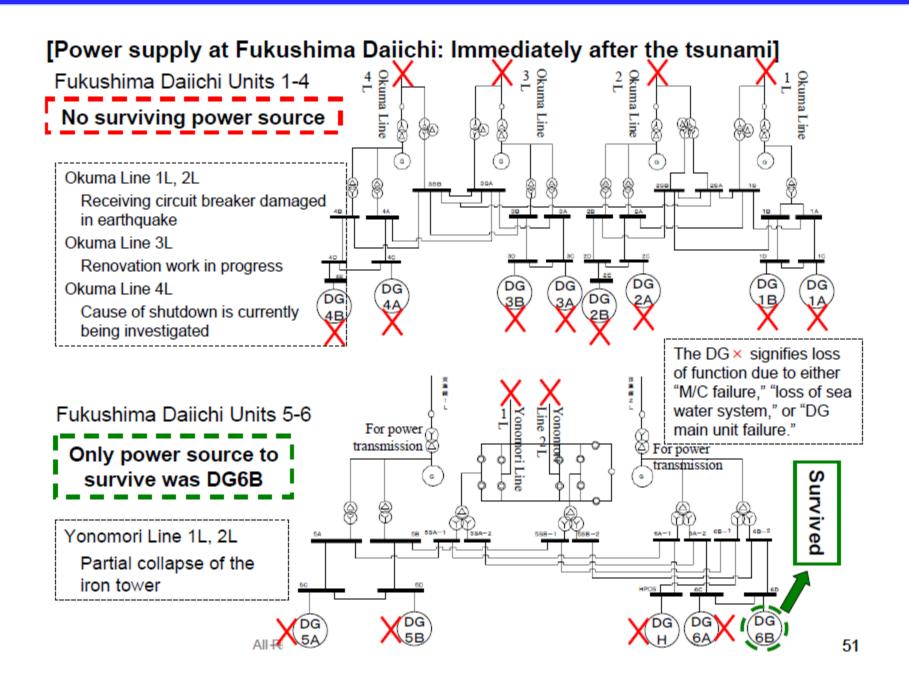


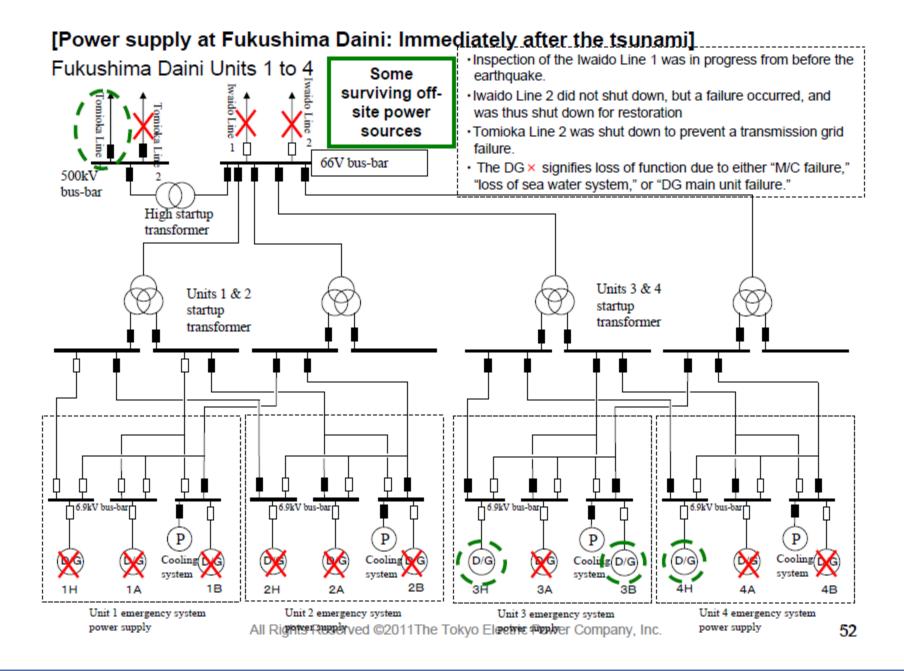


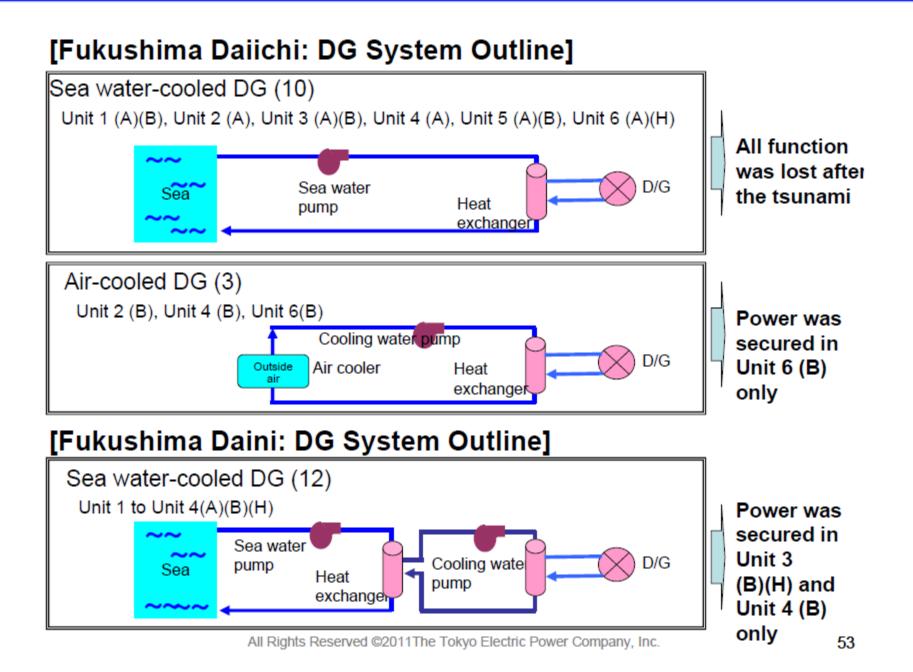
Tsunami damage at Fukushima Daini NPS

Daini









TSUNAMIS

4. Tsunami Hazard Assessment before 11 March 2011



Regulatory Guide for Reviewing Seismic Design of Nuclear Power Reactor Facilities 1. Introduction pp. 1 Scope of Application pp. 1 Basic Policy pp. 1 Classification of Importance in Seismic Design DD. 2 5. Determination of Design Basis Earthquake Ground Motion pp. 4 Principle of Seismic Design pp. 7 7. Load Combinations and Allowable Limits pp.12 8. Consideration of the Accompanying Events of Earthquake pp.14

Table of Contents

September 19, 2006. Nuclear Safety Commission

(URL:http://www.nsc.go.jp/english/taishin.pdf)

8. Consideration of the accompanying events of earthquake

Facilities shall be designed regarding the accompanying events of earthquake with sufficient consideration to the following terms.

 Safety functions of Facilities shall not be significantly affected by the collapses of the inclined planes around Facilities which could be postulated in the seismic events.

(2) Safety functions of Facilities shall not be significantly affected by the tsunami which could be postulated appropriately to attack but very scarcely in the operational period of Facilities.

Tsunami assessment in construction permit

site	unit	Permission year	rise	drawdown	Notes
Fukushima Daiichi NPS	1	1966	O.P. +3.122m Historic high water level	$O_{\rm P} = 1.919 m$	D.P. – 1.918m Height of the tide at Onahama port on May 24,1960 Chilean tsunami
	2	1968			
	3	1970			
	4	1972			
	5	1971		Historic low water level	
	6	1972			
Fukushima Daini NPS	1	1974			
	2	1 978	O.P.+3.690m	O.P. – 1.918m Historic low water level	O.P.+1.490m+2.2m=O.P.+3.690m 2.2m:height of the tsunami component at Onahma port on May 24,1960 Chilean tsunami O.P.+1.490m:Mean of high tides
	3	1980			O.P.+1.505m+2.2m=O.P.+3.705m
	4	1980	O.P.+3.705m	O.P. – 1.918m Historic low water level	2.2m:height of the tsunami component at Onahma port on May 24,1960 Chilean tsunami O.P.+1.505m:Mean of high tides

In those days, there was no tsunami assessment methodology based on numerical simulation for nuclear power plants.

JSCE Method

"Tsunami Assessment Method for Nuclear Power Plants in Japan (2002) "

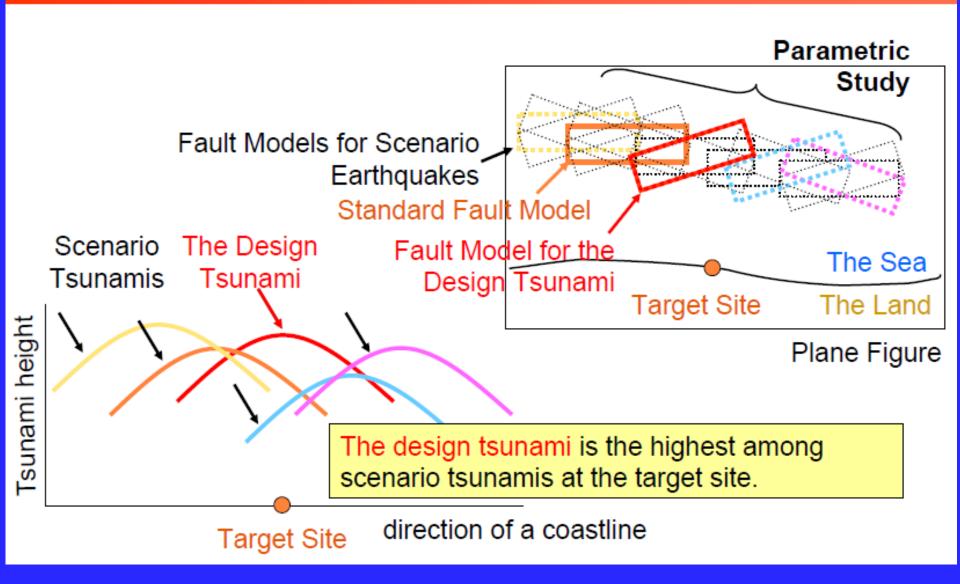
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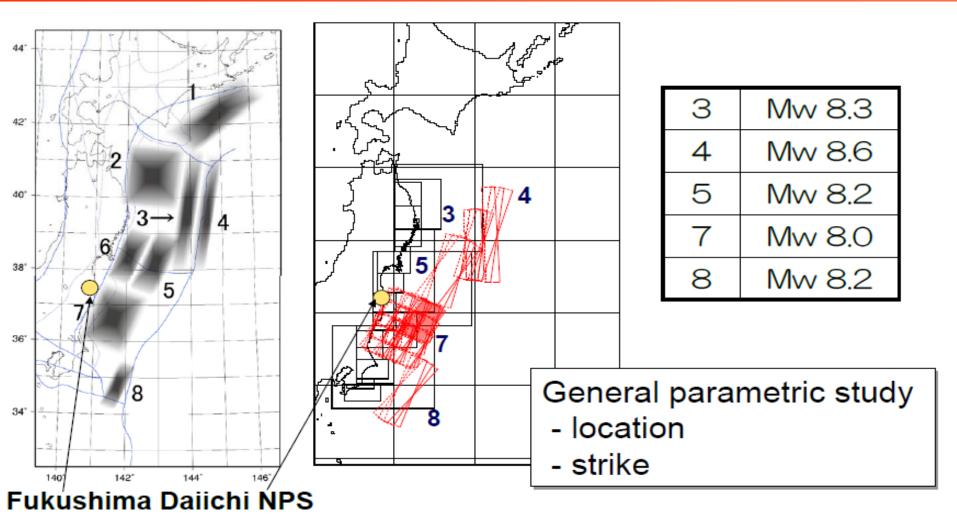
English version http://www.jsce.or.jp/committee/ceofnp/Tsunami/eng/tsunami_eng.html

Parametric Study of Tsunami Source



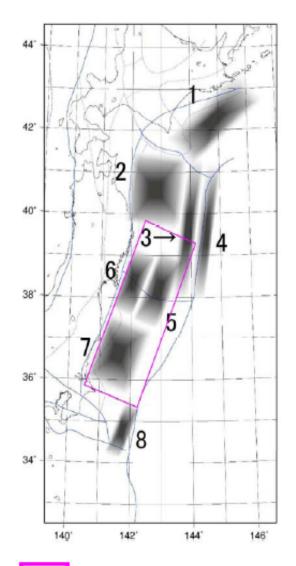
JSCE document indicates explicitly the seismogenic source areas to be adopted for the THA

General parametric study in the near field



Fukushima Daini NPS

The 2011 off the Pacific coast of Tohoku Earthquake



In JSCE 2002, earthquakes are assumed in 8 area individually. Earthquake on March 11th occurred cross over several areas.

No	Mvv	Earthquake
1	8.2	1952 Nemuro-oki
2	8.4	1968 Tokachi-oki
3	8.3	1896 Meiji-Sanriku
4	8.6	1611 Keicho-Sanriku
5	8,2	1793 Miyagi-oki
6	7.7	1978 Miyagi-oki
7	7.9	1938 Fukushima-oki
8	8.1	1677 Enpo-Bousou

2011/3/11 source area

(http://outreach.eri.u-tokyo.ac.jp/eqvolc/201103 tohoku/#Inversion 2011/3/18)

Consideration of tide and safety evaluation

The Design Tsunami

🔎 🦾 Tidal Conditions

Design High Water Level

= Maximum water rise + Mean of high tides

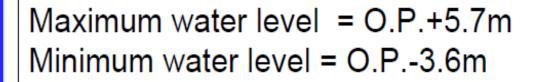
Design Low Water Level

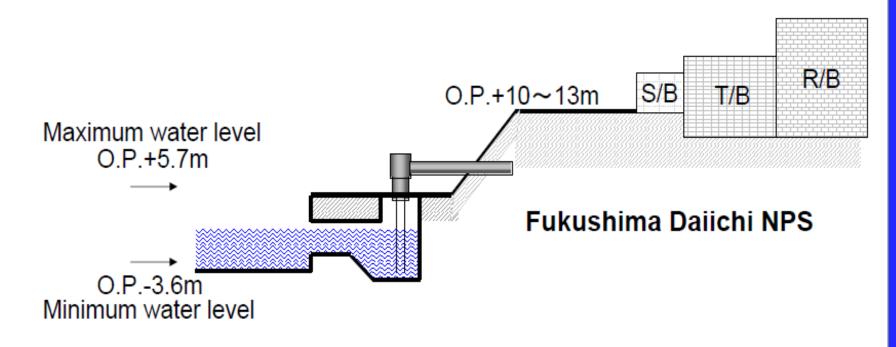
= Maximum water fall + Mean of low tides

Evaluation of the safety of NPP

RESULTS USING JSCE METHODOLOGY

Summary of Evaluation





- Although it appears that the Great East Japan earthquake exceeded the licensing based design basis ground motion of the F1 plant at the level of the foundation base mat in all units, the operating plants were automatically shutdown and all units behaved in a safe manner, during and immediately after the earthquake.
- It was also confirmed that in some cases the observed values even exceeded the recently determined maximum response acceleration values showing apparently an underestimation of the new DBGM Ss.

- The three fundamental safety functions of (a) reactivity control, (b) removal of heat from the core and (c) confinement of radioactive materials were available until the tsunami reached the sites.
- It is very difficult to separate earthquake damage from others in that situation; i.e. tsunami with extended flood, three explosions and possible thermal related failures due to sea water cooling (e.g. to the spent fuel pools from helicopters). As there was not enough time for a seismic walkdown in 45 minutes (before the tsunami came), it is not possible to rule out at least some damage due to the earthquake. However, the walkdown performed by US EPRI at F2 confirmed good performance and plant response to the earthquake. 76

- Based on the reports from Japanese experts and plant personnel, safety related structures, systems and components of the plant seemed to have behaved well for such a strong extreme earthquake, possibly due to conservatisms introduced at different stages of the design process. Similar to Kashiwazaki-Kariwa NPP experience and performance to NCO earthquake in 2007.
- The combined effects of these conservatisms were apparently sufficient to compensate for uncertainties in the data available and the methods applied at the time of the design of the plant and also the re-evaluated ground motions.

- The underestimation of the hazard in the original hazard study as well as in more recent re-evaluations mainly result from the use of recent historical seismological data in the estimation of the maximum magnitudes especially associated with the neighbouring subduction zone east of the sites.
- No consideration of higher magitudes already occurred in same seismotectonic environment, i.e. Pacific subduction rim.



LESSONS LEARNED - EARTHQUAKE

- It should be recognized worldwide the need to consider potential maximum seismic events greater than those observed or recorded in historical time.
- Although the need to consider pre-historical and historical data is well established in the international safety requirements for assessing the natural hazards at nuclear installations, this has not been followed especially in older nuclear power plants and in recent ones in which certain upper bounds to the maximum values are defined without proper consideration of experiences from time longer than recent historical records. Use of paleoseismology studies should be promoted.

LESSONS LEARNED - EARTHQUAKE

- The current IAEA safety standards establish a clear time scale (going back to historical and pre-historical eras) as well as tectonic capacity considerations in the estimation of maximum magnitudes associated with seismogenic structures.
- There is a need for Member States regulations to reflect these considerations both for the new build as well as for re-evaluation of existing NPPs.

LESSONS LEARNED - EARTHQUAKE

- Japan has undergone a seismic hazard re-evaluation (back check) recently on the basis of recent investigations and data. However, it was confirmed that these assessments were exceeded by the March 2011 event. This experience shows the importance of a permanent oversight of the potential hazards and of performing all required actions for taking necessary measures for maintaining and increasing the safety level.
- The Fukushima experience has also shown that there is a need to have in place a consistent and comprehensive pre-earthquake planning and post-earthquake response actions programme for all NPPs worldwide. IAEA has developed the new Safety Report 66 in this subject.

GENERAL OBSERVATIONS

- Operators and regulators need to make a greater effort to understand external hazards – external hazards should be treated as mainstream nuclear safety and not as an 'afterthought' – there is much room for progress in this area.
- For emergency preparedness, radiological emergency and a rare external hazard may occur together.

GENERAL OBSERVATIONS

- Suppliers should understand that "standard designs" for '0.25g' or '0.3g' are inadequate for many parts of the world – economic pressure in 'new build' countries to decrease hazard estimates (may have happened at F-1 in the 1960s).
- In the past 25 years:
 - Seismic hazard values increased by a factor of about 2
 - Maximum observed accelerations increased by about 4 (from 1g to 4g)
 - Standard seismic design values more or less stayed the same

GENERAL OBSERVATIONS

- All levels of Defense in Depth were challenged at the same time – concepts of redundancy, diversity and physical separation need to include external hazards.
- Safety analysis is performed for single unit whereas multi units and multi sites may be affected by a single external hazard.

 There were insufficient defence-in-depth provisions for tsunami hazards. Although tsunami hazards were considered both in the site evaluation and the design of the Fukushima Daiichi NPP and the expected tsunami height was later increased (without changing the licensing documents) after 2002, the tsunami hazard and associated risk was underestimated due to the underestimation of the maximum M magnitude associated with the subduction zone.



 Furthermore, considering that it was not possible to provide for a 'dry site' condition for these operating NPPs, the additional protective measures taken as result of the evaluation conducted after 2002 were not sufficient to cope with the unexpectedly higher tsunami run up values and all associated hazardous phenomena (hydrodynamic forces and impact of large debris).

Even the tectonic subsidence was not taken into account regarding the grade level to which the tsunami waves reached.

- Moreover, the re-evaluation of the hazard after 2002 and the adequacy of the protective actions taken were not reviewed and/or approved by the Regulatory Authority.
- Because failures of SSCs when subjected to floods are generally not incremental, the plants were not able to withstand the consequences of tsunami heights greater than those expected (cliff edge effect).

 The <u>tsunami warning and notification system</u>, if implemented and available, was not able to provide appropriate and timely response for plant reaction to the event. Japan, for example, has developed the TIPEEZ System which was not used as F1 plant and the operators were not aware of the coming of tsunami waves.

 It is recognized worldwide that Japan has a high level of expertise and also experience regarding tsunami hazard and provides leadership in this topic worldwide. This is reflected in the major influence that Japanese academic, scientific and technical institutions have on the international research and development of this topic.

It seems that organizational and governance issues have prevented this expertise to be applied to practical cases at the three NPPs affected.

- There is need to incorporate large safety factors to estimate tsunami run up for NPP sites for the following reasons:
- (i) large aleatory and epistemic uncertainties in parameters involved in tsunami hazard particularly the characterization of the tsunamigenic sources,
- (ii) significant variations in inundation levels at different parts of the site considering the specific and detailed plant layout and plant sector elevations,
- (iii)difficulties in incorporating effective tsunami protection measures for operating plants after an increase in tsunami height estimation,
- (iv)high vulnerability of NPP SSCs to increased flood levels, i.e. to flood related cliff edge effects.

- There is also need to use a systemic approach for dealing with the design and layout of the plant SSCs for an effective protection against tsunami hazards.
- Leak tightness and water resistance should be assured through a comprehensive evaluation of all potential water ways.
- However, this measure can only be used as a redundancy (i.e. in conjunction with a dry site or an effective site protection measure).

- For well defined tsunamigenic (fault controlled) sources, a large earthquake will always precede the tsunami. If the source is near the site, the vibratory ground motion will provide a warning.
- For all tsunamis that may occur at the site, notification from the national tsunami warning system should be transmitted to the control room for immediate operator actions.
- A clear procedure should be followed by plant management in preparing for a possible tsunami until the warning is lifted.

- An updating of regulatory requirements and guidelines should be performed reflecting the experience and data obtained during the Great East Japan Tsunami, using also the criteria and methods established in the IAEA related safety standards for comprehensively coping with tsunamis and in general all correlated external events.
- The national regulatory documents need to include data base requirements and assessment methodologies compatible with those required by IAEA Safety Standards.
- The methods for hazard estimation and the protection of the plant need to be compatible with the advances in research and development in this field.

- The potential for scenarios involving flooding hazards and multiple units (and possible multiple sites) needs to be fully and comprehensively investigated for new and existing nuclear power plants worldwide and if they cannot be screened out provisions for:
 - plant layout,
 - site protection measures,
 - design, accident management and emergency preparedness and response

should be taken in order to adequately protect the installation against these disasters.

 After a major disaster which may cause severe disruption to the plant the changed plant state and physical conditions of the SSCs need to be taken into consideration. The changed plant state (degraded systems and degraded physical conditions of the SSCs) may have lost design robustness and may have degraded defense in depth.

- The safety profile of the plant needs to be well understood (e.g. the required SSCs) for different plant states (e.g. shutdown) in order to provide for a consistent protection and a plan for upgrades.
- A major natural disaster may temporarily alter the environment at regional scale. In order to provide for an uninterrupted recovery process, there is a need for understanding the plant vulnerabilities and the new environment and providing protection for the plant and the recovery action accordingly in a timely manner.

There is a need to ensure that in considering external natural hazards the siting and design of nuclear plants should include sufficient protection against infrequent and complex combinations of external events and these should be considered in the plant safety analysis – specifically those that can cause site flooding and which may have longer term impacts;

There is a need to ensure that in considering external natural hazards:

 plant layout should be based on maintaining a 'dry site concept', where practicable, as a defense-in-depth measure against site flooding as well as physical separation and diversity of critical safety systems;

 common cause failure should be particularly considered for multiple unit sites and multiple sites, and for independent unit recovery options, utilizing all on-site resources should be provided;

FINAL REMARKS

- "one in one million it does not mean that is impossible";
- hazard assessment should be based on prehistorical and historical database;
- less complacent with human errors in the decision making process and the governance deficiencies;
- peer reviews by independent peers: effective way to learn and to generate changes and improvements
- was this accident preventable?

Thank you for your attention



Questions? agodoy@aon.at